

Mottier & Bell

A study of the loss
of head in gate valves

Civil Engineering

B. S.

1910

UNIVERSITY OF ILLINOIS
LIBRARY

Class

1910

Book

M858

Volume

Mr10-20M





100-11-11-11
156474

**A STUDY OF THE LOSS OF HEAD
IN GATE VALVES**

BY

CHARLES HALVATIOUS MOTTIER

AND

CHARLES MANLEY BELL

THESIS

FOR THE

DEGREE OF BACHELOR OF SCIENCE

IN

CIVIL ENGINEERING

COLLEGE OF ENGINEERING

UNIVERSITY OF ILLINOIS

PRESENTED JUNE, 1910

1913
M859



Digitized by the Internet Archive
in 2013

<http://archive.org/details/studyoflossoshea00mott>

1910
M858

UNIVERSITY OF ILLINOIS
COLLEGE OF ENGINEERING..

June 1, 1910

This is to certify that the thesis prepared in the Department of Theoretical and Applied Mechanics by CHARLES MANLY BELL and CHARLES HALVATIOUS MOTTIER entitled A Study of the Loss of Head in Gate Valves is approved by me as fulfilling this part of the requirements for the degree of Bachelor of Science in Civil Engineering.

Melvin L. Enger
Instructor in Charge

Approved:

AM Tabor
Professor of Municipal and Sanitary Engineering.
In Charge of Theoretical and Applied Mechanics.

Approved:

Ira O. Baker
Professor of Civil Engineering.

169151



TABLE OF CONTENTS

INTRODUCTION,	Page	1
METHOD OF EXPERIMENT,	Pages	2 - 3
RESULTS AND CONCLUSIONS,	Pages	9
TABLES,	Pages	10 - 19
PLATES,	Pages	20 - 24



INTRODUCTION.

The subject of this thesis was selected as one on which very little data was as yet available. After a long search for information on the subject it was found that four men had conducted experiments on the flow of water through gate valves. These four were Weisbach, Kuichling, Folwell and Thomas.

Weisbach conducted his experiments about thirty years ago on small valves up to about 2-1/2 inches in diameter; Kuichling investigated a large valve 24 inches in diameter; Folwell made a few experiments on a 4 inch gate valve and Thomas in a thesis for the degree of Bachelor of Science at the University of Illinois in 1906, tested one inch and two inch valves for the cause of loss of head. In view of the fact that nothing was as yet known regarding the loss of head in gate valves between 4 inches and 24 inches we decided to concentrate our efforts on valves 6 inches and over in diameter and if possible determine a law that would cover in a general way all sizes of valves.

The experiments were conducted in the Hydraulics Laboratory of the University of Illinois which has excellent facilities for carrying on such experiments.

METHOD OF EXPERIMENT.

Pressure was obtained from the sixty foot stand-pipe in the Laboratory, the level of water being kept constant at any height by a Snow Steam Pump with a Fisher altitude governor.

The water flowing from the stand-pipe, through the valve to be tested was discharged into a sump, from which it was again pumped into the stand-pipe. Thus the same water was used over and over again.

A 6 inch valve made by the Ludlow Valve Manufacturing Co., was first selected. The pipe leading from the valve emptied into an orifice box 4 ft. x 4-1/2 ft. x 6-1/2 ft. inside measurements, the valve being 2 ft. 6 in. from the end of the pipe which discharged into atmospheric pressure. A Bourdon gage was connected 6 in. below the valve, the reading on the gage giving the pressure head, which added to the elevation head gave the head lost in the valve and pipe. The head on the orifice was measured by a calibrated tube on one side of the box and the quantity calculated from the formula,

$$q = c F \sqrt{2 g H}$$

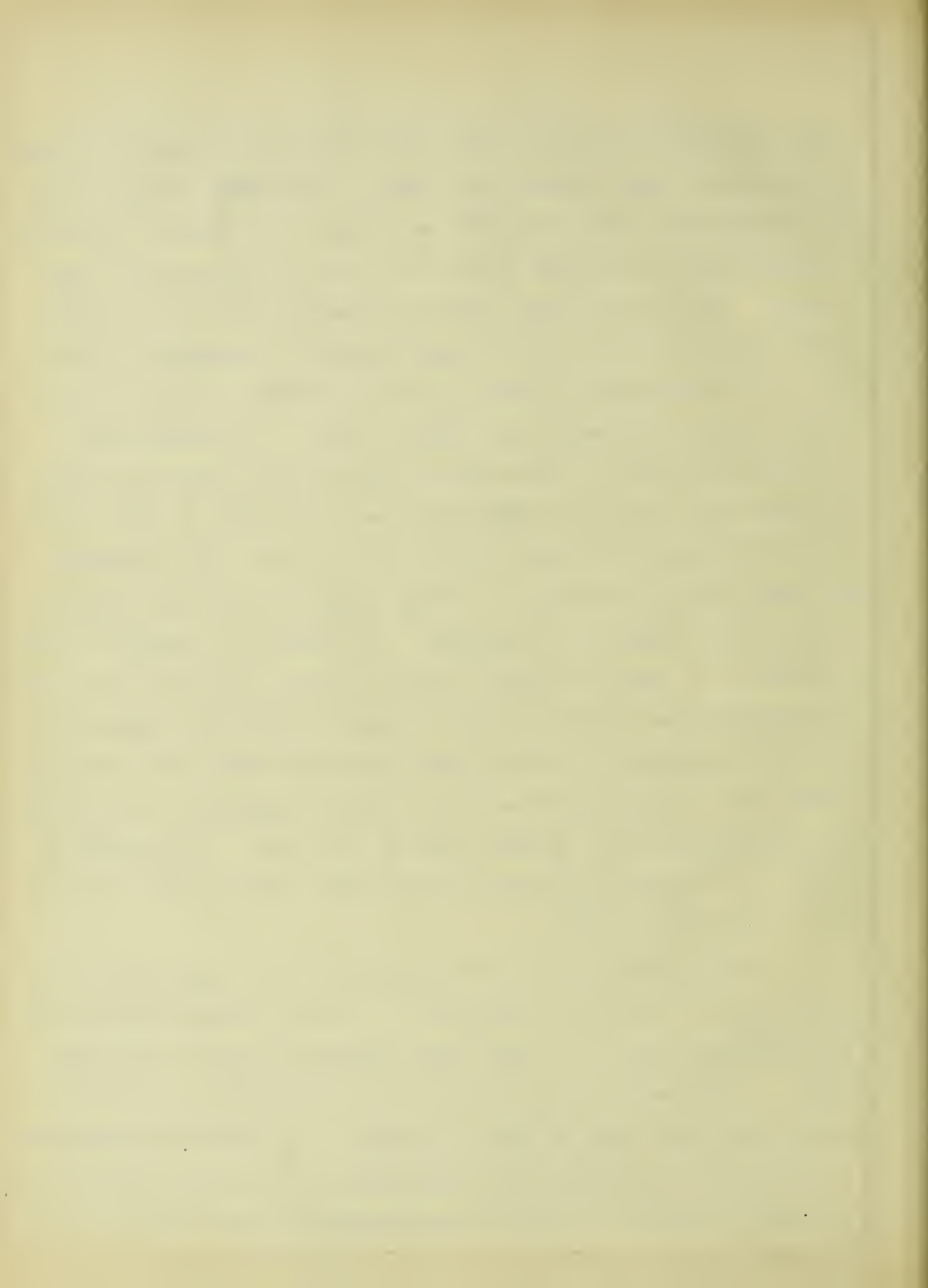
in which q is the quantity in cu. ft. per second, F the area of the orifice, H the height of water above the center of the orifice in feet, g the acceleration of gravity or 32.2 feet per second per second and c a constant depending upon the shape of the orifice and the height of water. The value of c was taken from tables in Merrimans Hydraulics. After a large number of readings had been

taken with the six inch orifice it was found that this size was not large enough to perform the experiments. It was therefore decided to abandon this method of procedure and adopt another which will now be described.

Another 6 inch valve made by the same company and situated on the south side of the basement of the laboratory was selected because it could be made to discharge into a large measuring pit about 5 feet and 8.02 feet in depth and diameter. The pipe on both sides of the valve for a considerable distance was horizontal which eliminated the necessity of taking into account any loss due to elevation. Two 1/4 inch holes were drilled in the pipe, one 2 feet above the valve and the other 18 feet below the valve. Into each hole was inserted a connection to which was attached a Bourdon gage. The elevation of the water in the pit was taken by means of a level rod at the beginning and end of a certain interval of time. The rod was first set at a certain point, the time being recorded when the water reached the rod. It was then raised a known distance and the time noted when the water again reached it. An ordinary Elgin watch was used to catch the time. The rate at which the water was discharged from the pipe was determined by multiplying the rise of the water by the cross-section area of the pit and dividing this result by the time. The loss of head in the pipe alone between the two pressure gages due to friction was calculated from Merriman's tables. The difference in the reading of the two pressure gages, after the loss in the pipe had been deducted, gave the loss due to the valve alone. The best method which we knew of to determine the percentage of opening of the valve was by finding the number of the

turns necessary to open the valve entirely and then count the number of turns each time a reading was taken. The number of turns necessary to open the valve completely was found to be $14\frac{1}{2}$. The valve was taken apart and it was found that 3 turns would open the valve 1 inch. Owing to the fact that the valve was forced into a seat after the opening was closed it was necessary to determine the number of turns required to raise the valve from its seat to the position at which water would just begin to flow. To obtain this, a $\frac{1}{4}$ " hole was bored in the bottom of the pipe just below the valve. The valve was then opened very slowly and the number of turns noted at just the moment the water ran out of the hole. This distance was found to be $1\frac{7}{8}$ turns. It was found that the valve could be turned $12\frac{7}{8}$ turns from this point. We therefore assumed the extra $\frac{7}{8}$ turn to be used in pulling the gate up into the hood of the valve. Measurements taken when the valve was apart checked our supposition and our observations. Before each reading was taken the valve was opened from a closed position to the required opening so as to avoid any motion lost in the backward turn of the valve. The number of turns in the tables and curves is the number from the point at which water just began to flow.

These results when plotted appeared to be inaccurate or at least did not follow any uniform law. It was therefore decided to discard these results and adopt more efficient methods of measurement. A stop watch was used in place of the ordinary watch to determine the exact time of flow in the pit. In the first experiments a great deal of difficulty was experienced in observing the elevation of water in the pit. The pipe discharging into one side of the pit



in an almost horizontal direction with a high velocity caused a swirling motion which in turn caused the water to rise on the sides of the pit higher than in the center. This was overcome in the later experiments by using a curved pipe which discharged the water vertically downward into the pit. The Bourdon pressure gages were discarded and in their place was used the differential pressure gage shown in the diagram Figure 2. The gage consisted of a U-tube half full of mercury. A rubber tube connected the top of one side of the gage to the pipe, being attached to the pipe 2-1/2 feet back of the center of the valve. A tube connected the top of the other side of the gage with the pipe 18-1/2 feet beyond the center of the valve. A stop cock was placed at the top of each side of the gage to permit any air to escape from the tubes. The scale was graduated to read the difference in pressure directly in feet. With these changes, the rest of the experiments were carried on and resulted in accurate data.

FIG. 1.

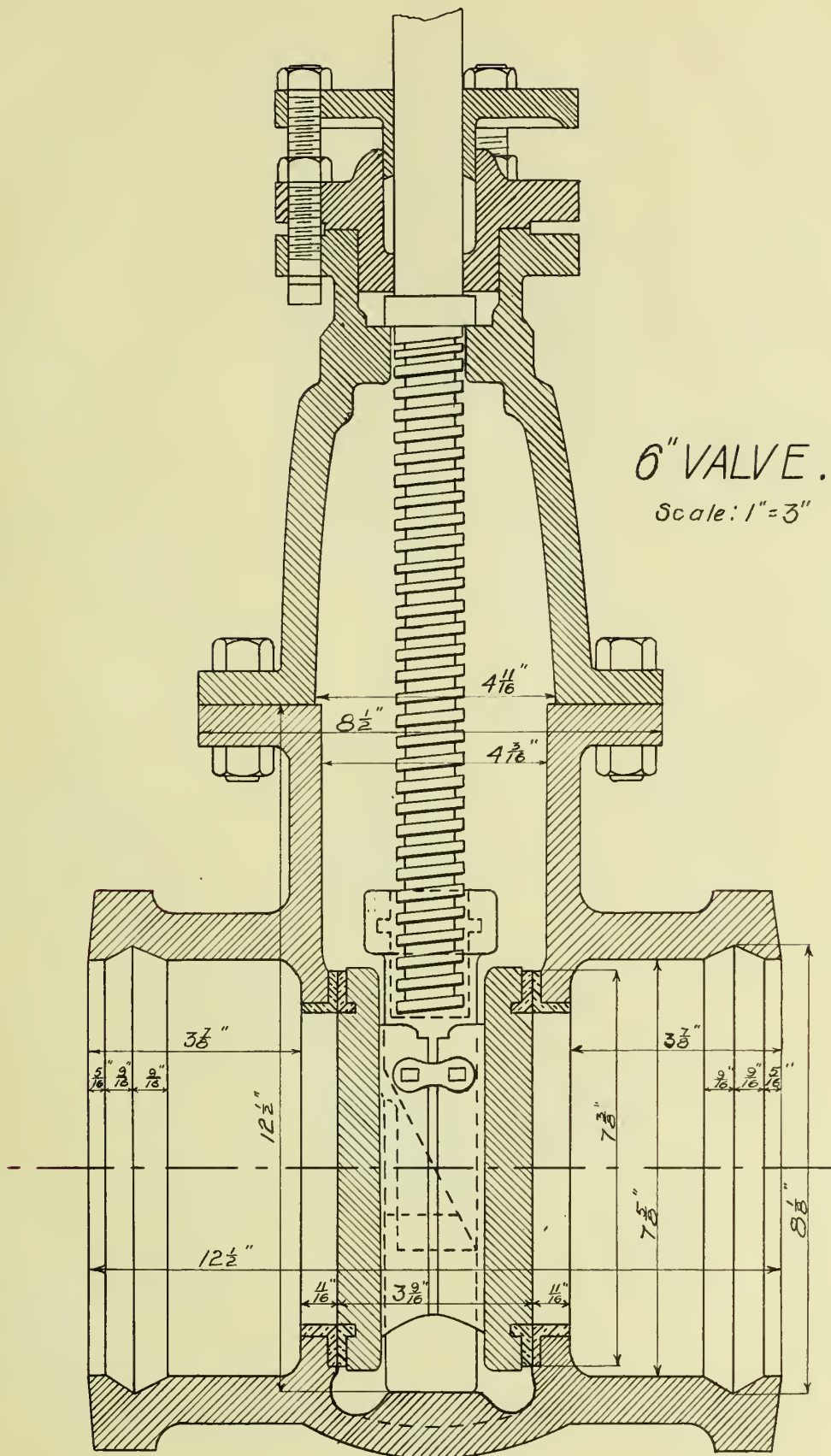
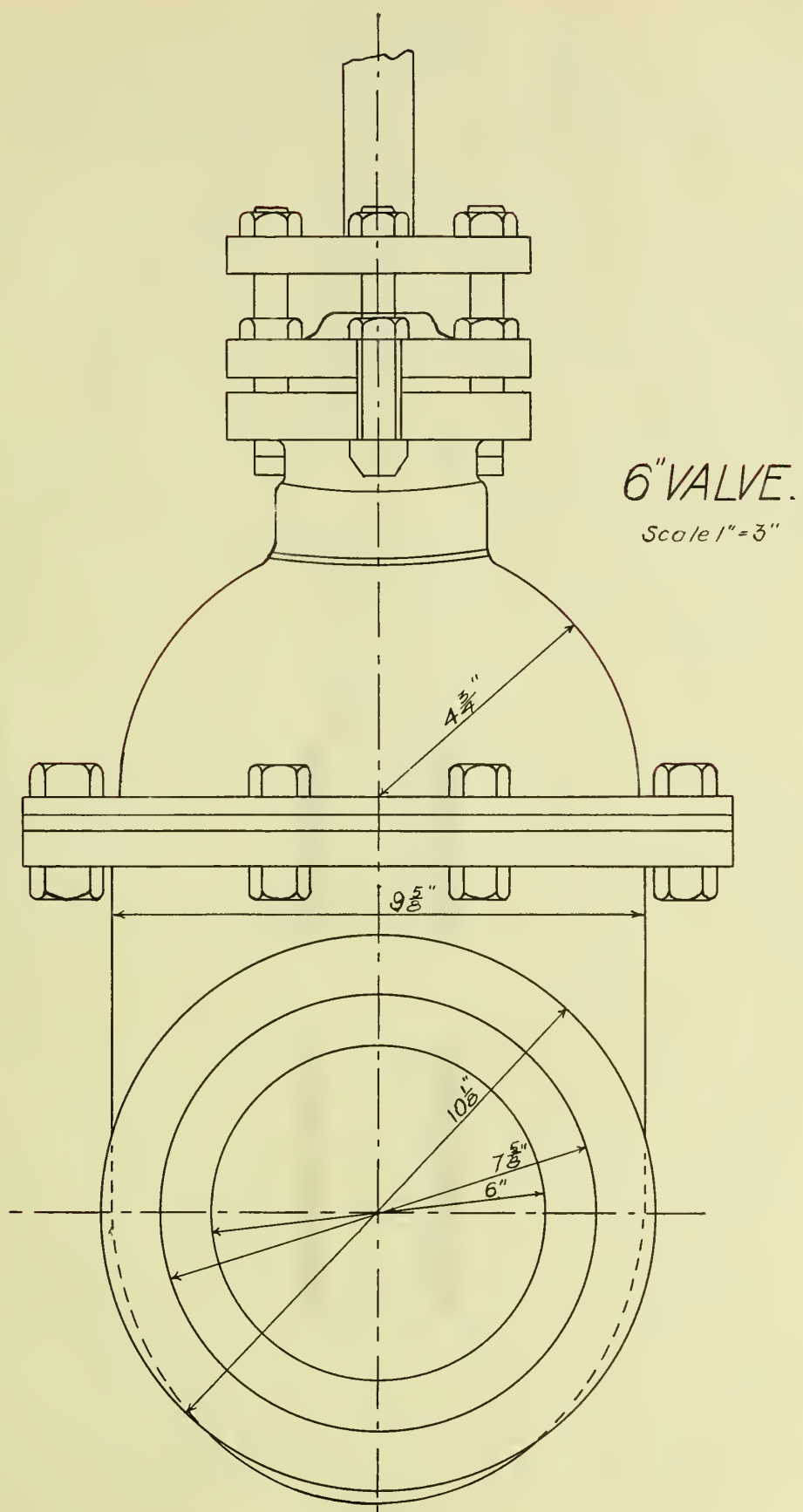




FIG. 2 .





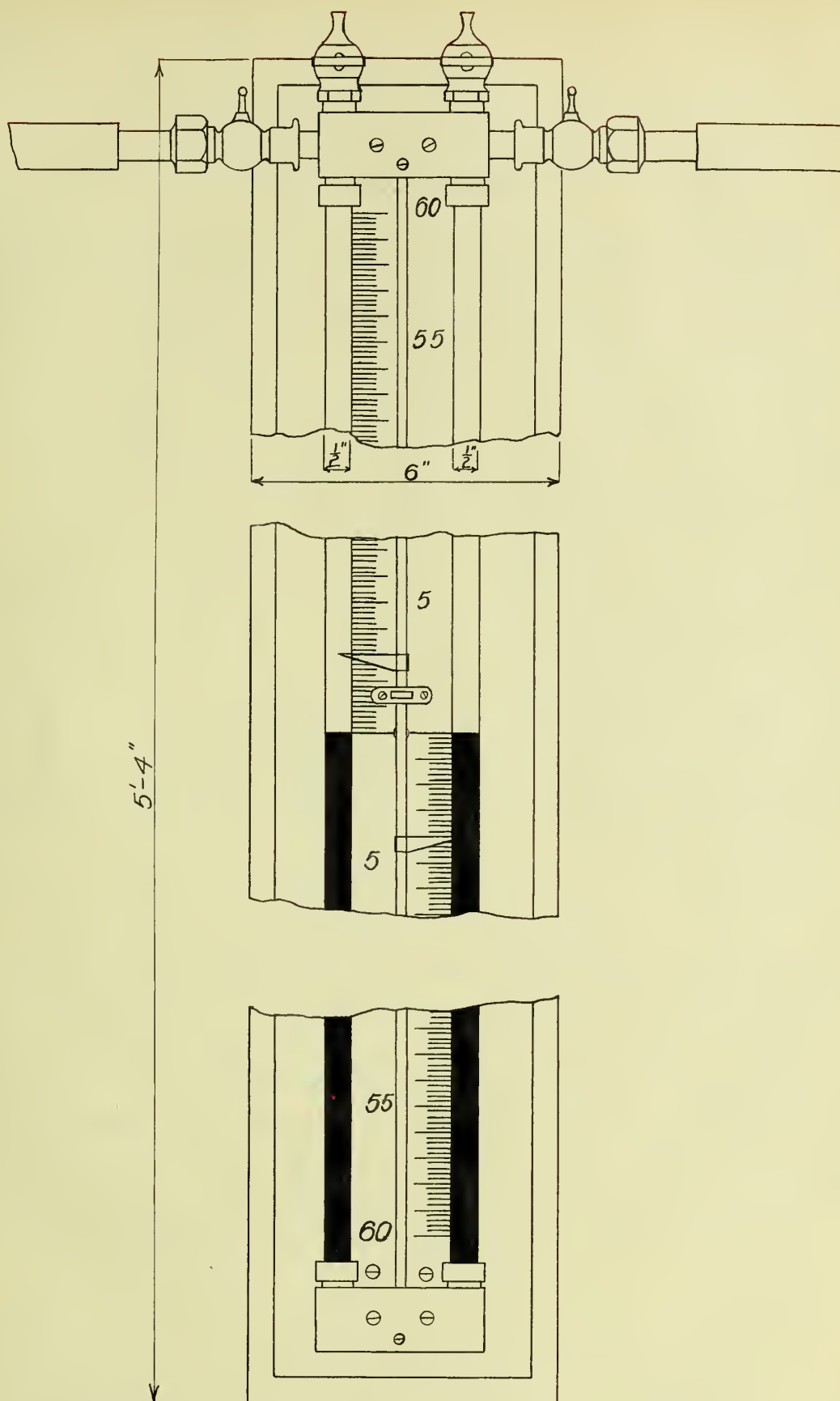


FIG. 3.

RESULTS AND CONCLUSIONS.

The average values of "m" in the equation $H = m \frac{v^2}{2g}$, as calculated from those in tables II and III, as well as those obtained by Kuichling and Weisbach in their experiments referred to in the introduction to this thesis are shown in the following table.

	Size of Valve	Ratio of Height of Opening to Diameter of Pipe							
		1	$\frac{7}{8}$	$\frac{3}{4}$	$\frac{5}{8}$	$\frac{1}{2}$	$\frac{3}{8}$	$\frac{1}{4}$	$\frac{1}{8}$
Kuichling	24"	0	—	1.0	1.5	3.3	8.6	22.7	75.5
Weisbach	2"	0	.07	.026	.081	2.1	5.5	17.0	98.0
Plate II	6"	1.0	1.1	1.4	2.5	4.0	8.7	21.0	116.0
Plate IV	8"	0	.03	.06	1.1	2.7	6.9	21.2	122.0

Plate V shows the agreement between the values found in these experiments and those of Weisbach and Kuichling.

These experiments also show the action of the valve in stopping the flow of water. It is seen from Plate V that very little loss takes place until the valve is $\frac{3}{4}$ closed. Beyond this point the loss increases very rapidly until the valve is completely shut. This shows that the valve can be over $\frac{3}{4}$ closed before any appreciable effect is noticed upon the flow of water through it.

TABLE I
DATA SHEET for 6" VALVE
USING BOURDON GAGES

No. of turns necessary to open valve = 12

$$H = m \frac{V^2}{2g}$$

Area of Pit = 51.54 sq. ft.; of pipe = 1.964 sq. ft.

Test No.	No. of Turns of Valve	Gage Readings				Rod Readings			Time Secs.	Discharge cu. ft. per sec.	Velocity Ft. per sec.	Loss in Friction in Pipe ft.	Loss in Valve ft.	m $\left(\frac{H}{\frac{V^2}{2g}}\right)$
		Gage No. 463 ft.	Gage No. 458 ft.	Gage No. 463 Corrected	Gage No. 458 Corrected	Difference in Readings	Initial ft.	Final ft.						
1	2	3	4	5	6	7	8	9	10	12	13	14	15	16
1	$\frac{1}{2}$	18.4	0	19.0	0	18.7	9.9	8.4	1.5	193	.982	.013	18.7	1330
14	$\frac{1}{2}$	25.5	0	25.9	0	25.8	10.3	8.3	2.0	202	1.02	.014	25.79	1720
26	$\frac{1}{2}$	31.1	0	31.2	0	30.4	10.9	7.7	3.2	224	1.14	.0186	30.38	1520
37	$\frac{1}{2}$	39.2	0	39.8	0	39.5	10.3	8.1	2.2	259	1.32	.0148	39.35	1400
48	$\frac{1}{2}$	35.1	0	35.2	0	35.2	9.6	7.9	1.7	237	1.21	.0157	35.18	1550
2	$\frac{1}{2}$	15.7	0	16.3	0	16.5	9.6	8.1	1.5	591	3.01	.131	16.4	116
15	$\frac{1}{2}$	22.1	0	22.5	0	22.4	10.4	7.4	3.0	715	3.64	.195	22.2	106
27	$\frac{1}{2}$	26.1	0	26.0	0	25.7	10.8	7.6	3.2	779	3.97	.223	25.5	106
38	$\frac{1}{2}$	34.8	0	35.0	0	34.8	9.5	7.2	2.3	830	4.23	.256	34.54	125
49	$\frac{1}{2}$	31.0	0	31.2	0	31.1	9.7	7.2	2.5	840	4.28	.259	30.8	110

TABLE I (cont'd)

Test No.	No. of Turns of Valve	Gage Readings				Rod Readings			Time Secs	Discharge Cu.ft. per Sec.	Velocity Ft. per Sec.	Loss in Friction in Pipe ft.	Loss in Valve ft.	m
		Gage No. 463 ft.	Gage No. 458 ft.	Gage No. 463 Corrected	Gage No. 458 Corrected	Difference in Readings	Initial ft.	Final ft.						
1	2	3	4	5	6	7	8	9	10	12	13	14	15	16
3	2½	13.0	0	13.6	0	13.6	9.0	7.5	1.5	.967	4.92	.346	13.30	35.7
16	2½	13.0	0	13.6	0	13.6	9.0	7.5	1.5	.967	4.92	.346	13.30	35.7
25	2½	17.2	0	17.8	0	17.8	10.0	7.5	2.5	1.072	5.45	.422	17.30	37.8
28	2½	17.0	0	17.5	0	17.5	10.0	7.5	2.5	1.072	5.45	.422	17.30	37.8
39	2½	3.1	0	3.4	0	3.4	9.5	7.5	2.0	.474	2.41	.835	1.965	22.0
50	2½	2.2	0	2.5	0	2.5	9.5	7.5	2.0	.474	2.41	.835	1.965	22.0
4	3½	20.4	0	20.7	0	20.7	9.8	7.3	2.5	1.228	6.25	.561	19.24	31.8
17	3½	18.6	0	19.0	0	19.0	9.8	7.3	2.5	1.228	6.25	.561	19.24	31.8
29	3½	27.5	0	27.5	0	27.5	9.8	7.5	2.3	1.395	7.10	.724	26.80	33.1
40	3½	27.5	0	27.5	0	27.5	9.8	7.5	2.3	1.395	7.10	.724	26.80	33.1
51	3½	23.8	0	23.9	0	23.9	9.4	7.4	2.0	1.34	6.80	.664	23.20	32.4
1	3½	23.8	0	23.9	0	23.9	9.4	7.4	2.0	1.34	6.80	.664	23.20	32.4
3	3½	8.9	0	9.5	0	9.5	8.7	7.2	1.5	1.228	6.24	.561	8.90	14.7
17	3½	8.9	0	9.5	0	9.5	8.7	7.2	1.5	1.228	6.24	.561	8.90	14.7
29	3½	12.5	0	13.1	0	13.1	10.0	7.5	2.5	1.302	6.62	.640	12.46	18.0
40	3½	12.5	0	13.1	0	13.1	10.0	7.5	2.5	1.302	6.62	.640	12.46	18.0
51	3½	16.0	0	16.5	0	16.5	10.0	7.3	2.7	1.530	7.79	.880	15.10	15.9
1	3½	15.0	0	15.5	0	15.5	10.0	7.3	2.7	1.530	7.79	.880	15.10	15.9
3	3½	21.0	0	21.0	0	21.0	9.8	7.4	2.4	1.670	8.50	1.040	19.96	17.5
17	3½	21.0	0	21.0	0	21.0	9.8	7.4	2.4	1.670	8.50	1.040	19.96	17.5
29	3½	18.9	0	18.9	0	18.9	9.2	7.2	2.0	1.640	8.35	1.000	17.90	16.6
40	3½	18.9	0	18.9	0	18.9	9.2	7.2	2.0	1.640	8.35	1.000	17.90	16.6
51	3½	18.9	0	18.9	0	18.9	9.2	7.2	2.0	1.640	8.35	1.000	17.90	16.6

TABLE I (cont'd)

Test No.	No. of Turns of Valve	Gage Readings				Rod Readings				Time Secs.	Discharge Cu.ft. per Sec.	Velocity Ft. per Sec.	Loss in Friction in Pipe ft.	Loss in Valve ft.	m
		Gage No. 463 ft.	Gage No. 458 ft.	Gage No. 463 Corrected	Gage No. 458 Corrected	Difference in Readings	Initial ft.	Final ft.	Difference ft.						
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16
43	6½	11.5	3.1	11.2	3.0										
		11.3	2.8	11.0	2.7	8.3	9.6	7.4	2.2	50	2.27	11.60	1.930	6.40	3.1
8	7½	3.0	0	3.2	0										
		3.0	0	3.2	0	3.2	9.45	7.45	2.0	64	1.610	8.18	.974	2.23	2.1
21	7½	5.2	0	5.5	0										
		5.2	0	5.5	0	5.5	9.4	7.4	2.0	56	1.840	9.36	1.260	4.20	3.1
33	7½	7.0	2.1	7.5	2.1										
		6.8	2.2	7.2	2.2	5.2	9.6	7.4	2.2	60	1.890	9.62	1.340	3.86	2.7
44	7½	9.9	3.9	9.8	3.8										
		9.7	3.5	9.6	3.4	6.1	9.6	7.5	2.1	48	2.26	11.50	1.900	4.20	2.1
9	8½	2.8	0	2.9	0										
		2.7	0	2.8	0	2.9	9.3	7.0	2.3	77	1.540	7.84	.891	2.00	2.1
22	8½	5.0	0	5.3	0										
		5.0	0	5.3	0	5.3	9.6	7.4	2.2	61	1.860	9.46	1.290	4.00	2.9
34	8½	5.9	2.3	6.2	2.3										
		5.8	2.3	6.1	2.3	3.8	9.6	7.4	2.2	54	2.100	10.70	1.650	2.15	1.2
45	8½	8.4	3.9	8.3	3.8										
		8.3	3.8	8.2	3.7	4.5	9.5	7.1	2.4	52	2.380	12.10	2.095	2.40	1.1
10	9½	2.3	0	2.3	0										
		2.4	0	2.4	0	2.4	9.5	7.0	2.5	82	1.572	8.00	.928	1.50	1.5
23	9½	4.6	1.8	5.0	1.8										
		4.5	1.8	4.9	1.8	3.2	9.6	7.4	2.2	60	1.890	9.61	1.34	1.86	1.3

TABLE I (cont'd)

Test No.	No. of Turns of Valve	Gage Readings				Rod Readings			Time Secs.	Discharge Cu. ft. per Sec.	Velocity Ft. per Sec.	Loss in Friction in Pipe ft.	Loss in Valve ft.	m
		Gage No. 463 ft.	Gage No. 458 ft.	Gage No. 463 Corrected	Gage No. 458 Corrected	Difference in Readings	Initial ft.	Final ft.						
1	2	3	4	5	6	7	8	9	10	12	13	14	15	16
35	9½	5.8	2.4	6.1	2.4									
		5.5	2.4	5.7	2.4	3.5	9.6	7.4	2.2	2.070	10.55	1.60	1.90	1.1
46	9½	7.8	3.9	7.8	3.8	4.0	9.5	7.3	2.2	2.270	11.60	1.93	2.10	1.0
		7.7	3.8	7.7	3.7									
12	12	2.1	0	2.1	0	2.2	9.4	7.0	2.4	1.548	7.86	.891	1.30	1.3
		2.2	0	2.2	0									
24	12	4.4	1.9	4.8	1.9	2.9	9.5	7.4	2.1	1.900	9.67	1.35	1.55	1.0
		4.4	1.9	4.8	1.9									
36	12	5.4	2.5	5.6	2.5	3.1	9.5	7.4	2.1	2.22	11.30	1.85	1.25	0.6
		5.4	2.5	5.6	2.5									
47	12	7.2	3.0	7.2	2.9	4.3	9.4	7.4	2.0	3.04	15.50	3.46	0.8	0.2
		7.2	3.0	7.2	2.9									

4 31

1.0

6

7.2

11.8

.6

TABLE II
DATA SHEET for 6" VALVE
USING DIFFERENTIAL PRESSURE GAGE.

$$H = m \frac{V^2}{2g}$$

Area of Pit = 51.54 sq.ft.; of Pipe = 1964 sq.ft.

No. of Turns necessary to open valve = 12

Test No.	No. of Turns of Valve	Gage Readings			Rod Readings			Time Secs.	Discharge cu.ft. per sec.	Velocity Ft. per sec.	Velocity Head $\left(\frac{V^2}{2g}\right)$	Loss in Friction in Pipe. ft	Loss in Valve ft	m
		R ₁ ft.	R ₂ ft.	Average ft.	Initial ft.	Final ft.	Difference ft							
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
57	1½	5.7	6.9	6.3	10.6	7.6	3.0	468	331	1.685	.045	.0396	6.3	140
61	1½	6.8	8.4	7.6	10.5	7.5	3.0	438	354	1.800	.060	.0528	7.6	127
64	1½	1.8	2.4	2.1	10.5	7.5	3.0	541	286	1.455	.035	.0308	2.1	60
65	1½	7.8	6.5	7.2	10.5	7.5	3.0	401	386	1.965	.064	.0563	7.2	113
66	1½	6.4	7.6	7.0	10.5	7.5	3.0	407	381	1.940	.060	.0528	7.0	117
73	1½	17.8	19.8	18.8	9.4	7.4	2.0	154	669	3.400	.160	.140	18.7	117
81	1½	36.6	30.8	33.7	10.1	7.1	3.0	180	860	4.370	.295	.260	33.4	113
89	1½	49.7	42.0	45.8	10.1	7.1	3.0	151	1,025	5.740	.510	.450	45.2	89
97	1½	28.9	34.8	31.8	9.6	7.6	2.0	124	832	4.240	.280	.240	31.6	113
98	1½	31.0	37.1	34.1	9.3	7.3	2.0	119	866	4.410	.300	.260	33.8	106?
99	1½	13.6	15.8	14.7	9.5	7.3	2.2	217	523	2.660	.110	.100	14.5	132
107	1½	26.3	22.2	24.1	9.3	7.3	2.0	143	721	3.670	.207	.180	23.9	115
115	1½	25.8	22.0	23.9	9.2	7.2	2.0	143.5	719	3.660	.207	.180	23.7	114
58	3	1.6	1.2	1.4	10.6	7.6	3.0	415	374	1.905	.060	.0528	1.4	234
62	3	1.0	0.6	0.8	10.5	7.5	3.0	600	248	1.262	.025	.0220	0.8	32.0
67	3	1.0	1.2	1.1	10.5	7.2	3.3	348	490	2.495	.096	.0844	1.1	11.5
74	3	14.8	13.0	13.9	8.35	6.95	1.4	56	1,285	6.56	.670	.590	13.3	199
82	3	24.4	21.1	22.8	9.0	7.1	1.9	61	1,605	8.19	1.04	.92	21.9	21.0
90	3	28.6	34.0	31.3	10.1	7.1	3.0	82	1,888	9.62	1.44	1.28	30.0	208
100	3	8.4	10.0	9.2	9.3	7.3	2.0	104	992	5.05	.395	.34	8.9	26.2

TABLE II (cont'd)

Test No.	No. of Turns of Valve	Gage Readings			Rod Readings			Time Secs.	Discharge Cu.ft. per Sec.	Velocity Ft. per Sec.	Velocity Head $\frac{v^2}{2g}$	Loss in Friction in Pipe ft.	Loss in Valve ft.	m
		R ₁ ft.	R ₂ ft.	Average ft.	Initial ft.	Final ft.	Difference ft.							
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
108	3	16.4	18.8	17.6	9.3	7.3	2.0	74	1.392	7.09	.78	.68	16.9	21.6
59	4½	0.5	1.0	.75	10.6	7.5	3.1	375	.427	2.175	.073	.068	0.68	9.3
63	4½	0.8	0.4	0.6	10.5	7.5	3.0	579	.267	1.36	.030	.0264	0.60	22.7
68	4½	0.7	0.5	0.6	10.5	7.5	3.00	378	.410	2.086	.070	.0616	0.60	9.7
75	4½	7.8	9.8	8.8	9.2	7.2	2.0	66	1.56	7.94	.98	.863	7.9	8.1
83	4½	15.5	13.4	14.5	9.3	7.2	2.1	57	1.90	9.66	1.45	1.28	13.2	9.1
91	4½	20.6	18.9	19.8	9.9	7.2	2.7	61	2.28	11.60	2.03	1.78	18.0	8.9
101	4½	6.5	7.4	6.9	9.3	7.3	2.0	77	1.34	6.825	.072	.63	6.3	8.8
109	4½	9.9	11.6	10.7	9.3	7.3	2.0	61	1.691	8.605	1.16	1.01	9.7	8.4
60	6	0.2	0.4	0.3	10.6	7.6	3.0	288	.538	2.74	0.011	0.101	0.2	1.8
69	6	0.3	0.6	0.5	10.5	8.3	2.2	276	.408	2.08	0.070	0.062	0.4	5.7
76	6	5.6	4.8	5.2	9.5	7.3	2.2	66	1.74	8.75	1.18	1.04	4.2	3.6
84	6	10.0	8.5	9.3	9.5	7.2	2.3	55	2.16	11.00	1.88	1.65	7.6	4.0
92	6	13.5	11.8	12.6	9.7	7.2	2.5	51	2.53	12.89	2.51	2.25	10.3	4.1
102	6	3.6	4.4	4.0	9.3	7.3	2.0	68	1.516	7.72	.92	.80	3.2	3.5
110	6	6.4	7.3	6.8	8.9	6.9	2.0	54	1.910	9.73	1.47	1.28	5.6	3.8
70	7½	0.3	0.3	0.3	10.5	7.5	3.0	360	.430	2.19	0.08	.0704	0.3	3.7
77	7½	4.2	3.8	4.0	9.3	7.3	2.0	57	1.81	9.20	1.315	1.160	2.8	2.1
85	7½	7.0	6.4	6.7	9.3	7.3	2.0	47	2.195	11.19	1.91	1.68	5.0	2.6
93	7½	10.2	8.8	9.5	9.5	7.3	2.2	43	2.64	13.45	2.73	2.40	7.1	2.6
103	7½	2.6	3.2	2.9	9.3	7.3	2.0	66.5	1.550	7.89	.97	.84	2.2	2.3

TABLE II (contd)

Test No.	No of Turns of Valve	Gage Readings			Rod Readings			Time Secs.	Discharge Cu.ft. per Sec.	Velocity Ft. per Sec.	Velocity Head $\frac{V^2}{2g}$	Loss in Friction in Pipe ft.	Loss in Valve ft.	m
		R. ft.	R ₂ ft.	Average ft.	Initial ft.	Final ft.	Difference ft.							
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
78	9	3.6	3.4	3.5	9.3	7.3	2.0	56	1.84	9.36	1.36	1.20	2.3	1.7
86	9	4.6	4.1	4.35	9.3	7.1	2.2	49	2.315	11.70	2.06	1.81	2.5	1.2
94	9	7.6	6.6	7.1	9.3	7.3	2.0	37	2.79	14.20	3.12	2.75	4.4	1.4
104	9	2.6	2.1	2.3	9.1	7.1	2.0	65	1.588	8.08	1.015	.88	1.4	1.4
112	9	3.4	4.0	3.7	9.2	7.2	2.0	51.5	2.005	10.20	1.56	1.36	2.4	1.8
79	10½	3.1	2.8	2.95	10.2	7.3	2.9	84	1.780	9.05	1.27	1.12	1.8	1.4
87	10½	4.6	3.9	4.25	9.3	7.1	2.2	49	2.315	11.70	2.06	1.81	2.4	1.2
95	10½	6.6	5.4	6.0	9.3	7.3	2.0	37	2.790	14.20	3.12	2.75	3.3	1.1
105	10½	2.3	1.8	2.0	9.3	7.3	2.0	64	1.610	8.195	1.04	.88	1.1	1.1
113	10½	2.9	3.4	3.15	9.2	7.2	2.0	50.5	2.042	10.40	1.57	1.37	1.8	1.2
80	12	3.0	2.8	2.9	9.8	7.3	2.5	71	1.82	9.26	1.33	1.51	1.4	1.0
88	12	4.6	3.8	4.2	9.3	7.2	2.1	46	2.465	12.52	2.36	2.08	2.1	0.9
96	12	6.2	5.3	5.75	9.3	7.3	2.0	37	2.790	14.20	3.12	2.75	3.0	1.0
106	12	2.3	1.8	2.0	9.3	7.3	2.0	61	1.691	8.605	1.16	1.01	1.0	0.9
114	12	2.8	3.3	3.05	9.2	7.2	2.0	51.	2.022	10.30	1.565	1.36	1.7	1.3

TABLE III
DATA SHEET for 8" VALVE
USING DIFFERENTIAL PRESSURE GAGE

$$H = m \frac{V^2}{2g}$$

Area of Pit = 51.54 sqft.; of Pipe =

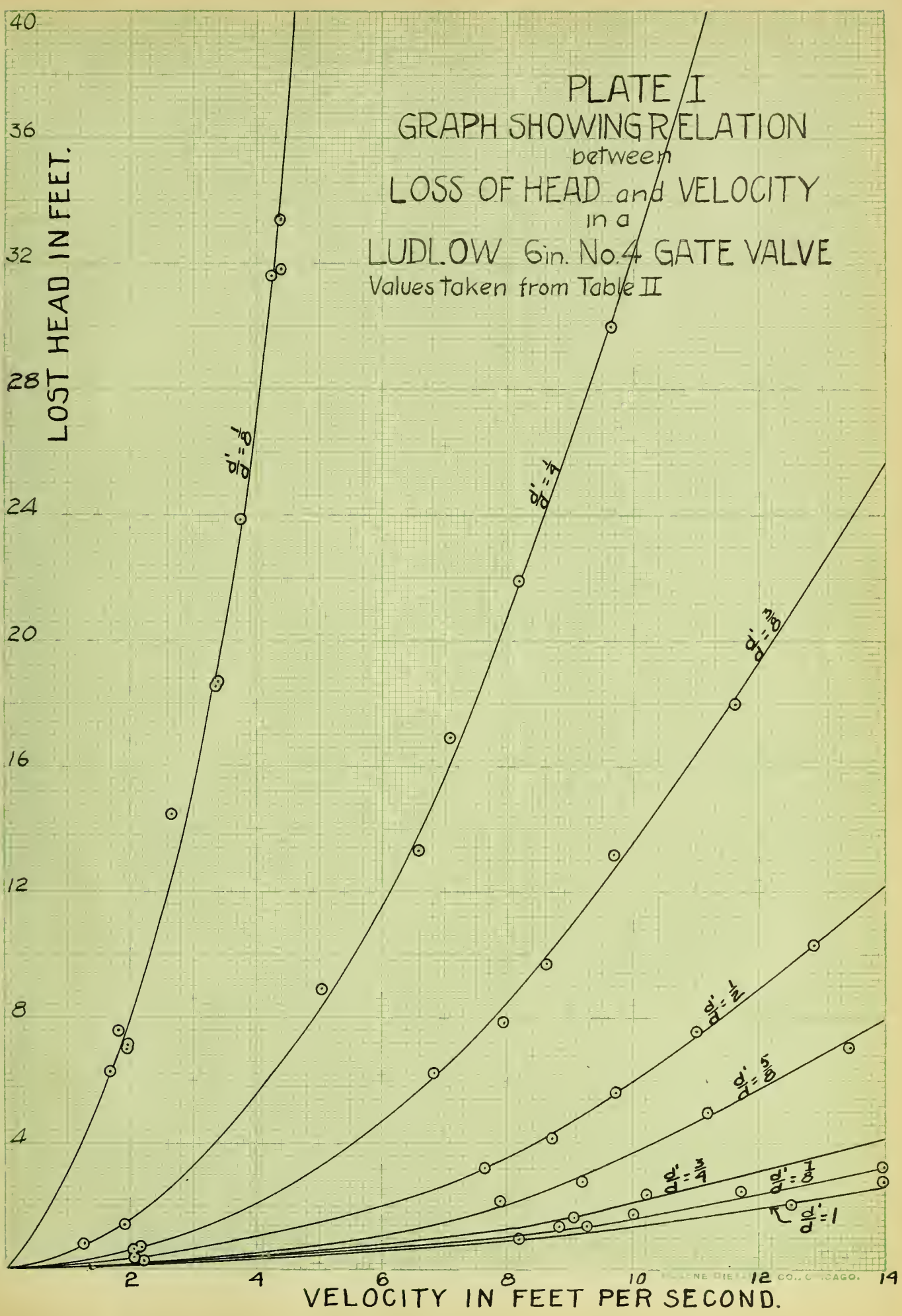
No. of turns necessary to open valve = 16

Test No.	No. of Turns of Valve	Gage Readings			Rod Readings			Time Secs.	Discharge Cuft. per sec.	Velocity Ft. per sec.	Velocity Head $\frac{V^2}{2g}$	Loss in Friction in Pipe ft.	Loss in Valve ft.	m
		R ₁ ft.	R ₂ ft.	Average ft.	Initial ft.	Final ft.	Difference ft.							
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
5	2	24.2	28.5	26.35	10.0	7.5	2.5	97.0	1.33	3.81	2.2	.03	26.3	120
13	2	32.0	38.0	35.0	10.0	7.5	2.5	87.5	1.47	4.21	2.8	.04	35.0	125
29	2	12.0	14.1	13.05	10.0	7.5	2.5	146.0	.884	2.53	.10	.01	13.0	130
36	2	2.9	2.6	2.75	9.5	8.5	1.0	124.0	4.16	1.19	.02	.00	2.6	130
41	2	6.7	7.4	7.05	9.8	8.8	1.0	76.5	.675	1.935	.06	.00	7.0	117
6	4	11.4	13.2	12.3	10.0	7.5	2.5	60.0	2.15	6.15	.59	.08	12.2	20.7
14	4	15.2	17.6	16.4	10.0	7.5	2.5	52.0	2.48	7.10	.78	.09	16.3	20.9
22	4	19.3	22.8	21.05	10.0	7.5	2.5	46.5	2.77	7.93	.98	.13	20.9	21.3
30	4	20.5	23.9	22.2	10.0	7.5	2.5	46.0	2.80	8.02	1.00	.13	22.1	22.1
37	4	0.7	0.7	0.7	10.0	9.0	1.0	106.5	0.485	1.39	.03	.00	0.7	23.4
43	4	11.7	13.5	12.6	9.5	7.5	2.0	48.0	2.15	6.15	.59	.08	12.5	21.2
7	6	5.8	5.4	5.6	10.0	7.5	2.5	50.5	2.55	7.31	.83	.11	5.5	6.6
15	6	6.5	7.7	7.1	10.0	7.5	2.5	45.0	2.86	8.19	1.04	.14	7.0	6.7
23	6	8.3	9.8	9.05	10.0	7.5	2.5	41.0	3.14	9.00	1.26	.17	8.8	7.0
31	6	9.0	10.3	9.65	10.0	7.5	2.5	38.0	3.49	10.00	1.55	.21	9.4	6.1
38	6	1.3	1.3	1.3	9.5	7.5	2.0	87.5	1.18	3.38	.18	.02	1.3	7.2
44	6	2.0	2.0	2.0	9.5	7.5	2.0	70.0	1.47	4.21	.28	.04	2.0	7.1
8	8	1.4	1.4	1.4	10.0	7.5	2.5	48.0	2.68	5.67	.50	.07	1.3	2.6
16	8	3.0	3.4	3.2	10.0	7.5	2.5	43.5	2.96	8.48	1.11	.15	3.0	2.7
24	8	3.4	3.9	3.65	10.0	7.5	2.5	39.0	3.31	9.46	1.39	.15	3.5	2.5

TABLE III (contd)

Test No.	No. of Turns of Valve	Gage Readings			Rod Readings		Time Secs.	Discharge Cu.ft. per Sec.	Velocity Ft. per Sec.	Velocity Head $\frac{V^2}{2g}$	Loss in Friction in Pipe ft.	Loss in Valve ft.	m	
		R ₁ ft.	R ₂ ft.	Average ft.	Initial ft.	Final ft.								Difference ft.
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
32	8	4.0	4.6	4.3	9.5	7.5	2.0	29.5	3.50	10.0	1.55	.21	4.1	2.6
39	8	0.9	0.9	0.9	9.5	7.5	2.0	66.5	1.55	4.44	.305	.04	0.9	2.9
17	10	1.6	1.6	1.6	10.0	7.5	2.5	41.5	3.11	8.91	1.23	.16	1.4	1.1
25	10	1.8	1.8	1.8	10.0	7.5	2.5	37.5	3.44	9.85	1.51	.16	1.6	1.0
33	10	2.2	2.2	2.2	9.5	7.5	2.0	29.5	3.50	10.00	1.55	.21	2.0	1.3
40	10	0.5	0.5	0.5	9.5	7.5	2.0	65.5	1.58	4.53	.32	.04	0.5	1.6
10	12	-0.1	-0.1	-0.1	10.0	7.5	2.5	47.0	2.74	7.85	.96	.13	0.0	0.0
18	12	0.9	0.9	0.9	10.0	7.5	2.5	41.0	3.14	9.00	1.26	.17	0.7	0.6
26	12	0.7	0.7	0.7	10.0	7.5	2.5	37.5	3.44	9.85	1.51	.16	0.5	0.3
34	12	1.2	1.2	1.2	9.5	7.5	2.0	29.5	3.50	10.00	1.55	.21	1.0	0.6
11	14	-0.5	-0.5	-0.5	10.0	7.5	2.5	47.0	2.74	7.85	.96	.13	0.0	0.0
19	14	0.5	0.5	0.5	10.0	7.5	2.5	41.5	3.11	8.91	1.23	.16	0.3	0.2
27	14	0.1	0.1	0.1	10.0	7.5	2.5	37.5	3.44	9.85	1.51	.16	0.0	0.0
35	14	0.6	0.6	0.6	9.5	7.5	2.0	29.5	3.50	10.00	1.55	.21	0.4	0.3
12	16	-0.6	-0.6	-0.6	10.0	7.5	2.5	47.0	2.74	7.85	.96	.13	0.0	0.0
20	16	0.3	0.4	0.35	10.0	7.5	2.5	41.0	3.14	9.00	1.26	.17	0.2	0.2
28	16	-0.1	-0.1	-0.1	10.0	7.5	2.5	37.5	3.46	9.91	1.53	.20	0.0	0.0

PLATE I
 GRAPH SHOWING RELATION
 between
 LOSS OF HEAD and VELOCITY
 in a
 LUDLOW 6in. No. 4 GATE VALVE
 Values Taken from Table II



17-11

PLATE II
 GRAPHS SHOWING RELATION
 BETWEEN
 LOSS OF HEAD AND VELOCITY HEAD
 IN A
 LUDLOW 6 IN. NO. 4 GATE VALVE
 Values taken from Table II

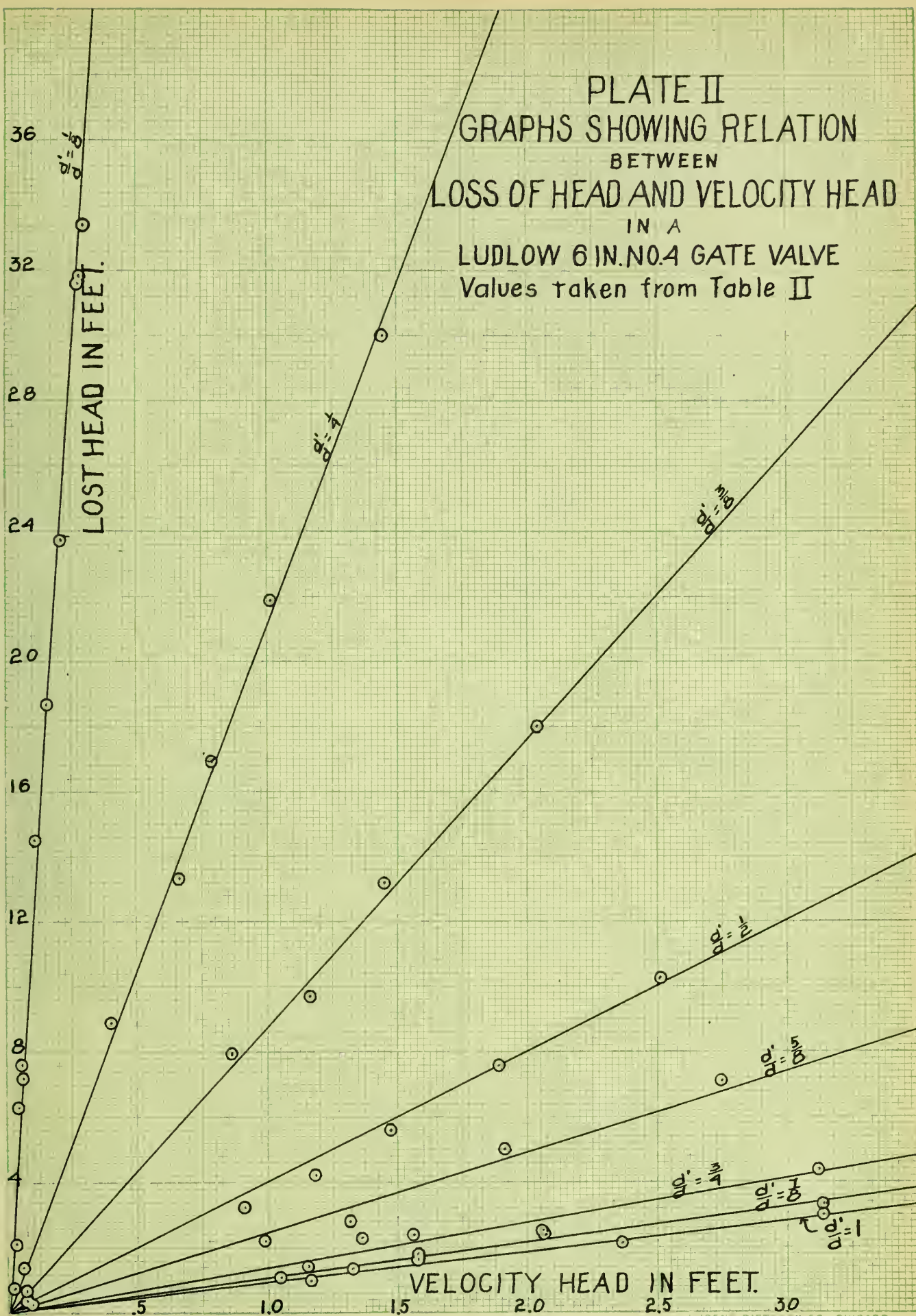


PLATE III
 GRAPH SHOWING RELATION
 BETWEEN
 LOSS OF HEAD AND VELOCITY
 IN A
 LUDLOW 8 IN. NO. 4 GATE VALVE
 Values taken from Table III.

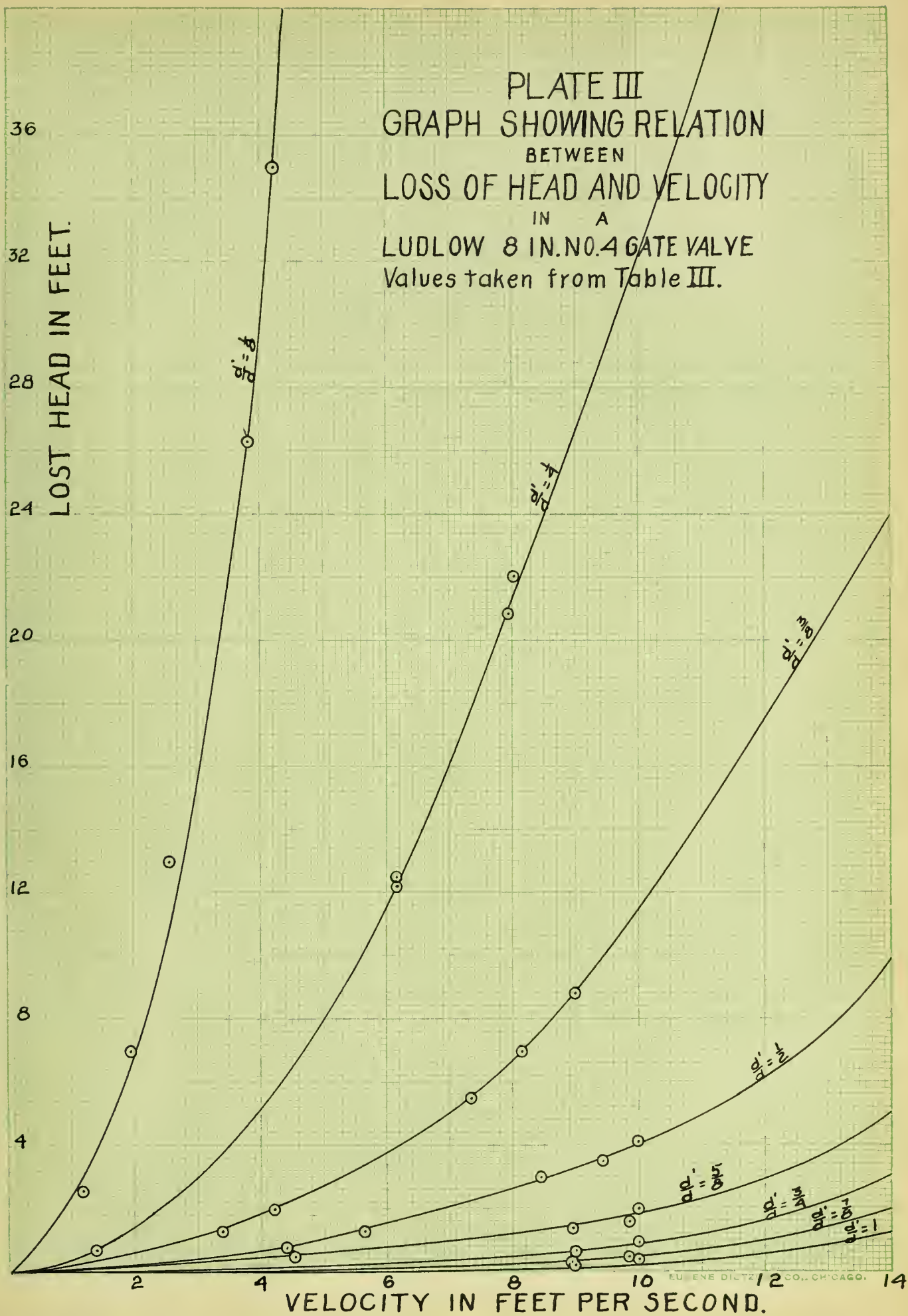


PLATE IV
 GRAPHS SHOWING RELATION
 BETWEEN
 LOSS OF HEAD AND VELOCITY HEAD
 IN A
 LUDLOW 8 IN. NO. 4 GATE VALVE
 Values taken from Table III.

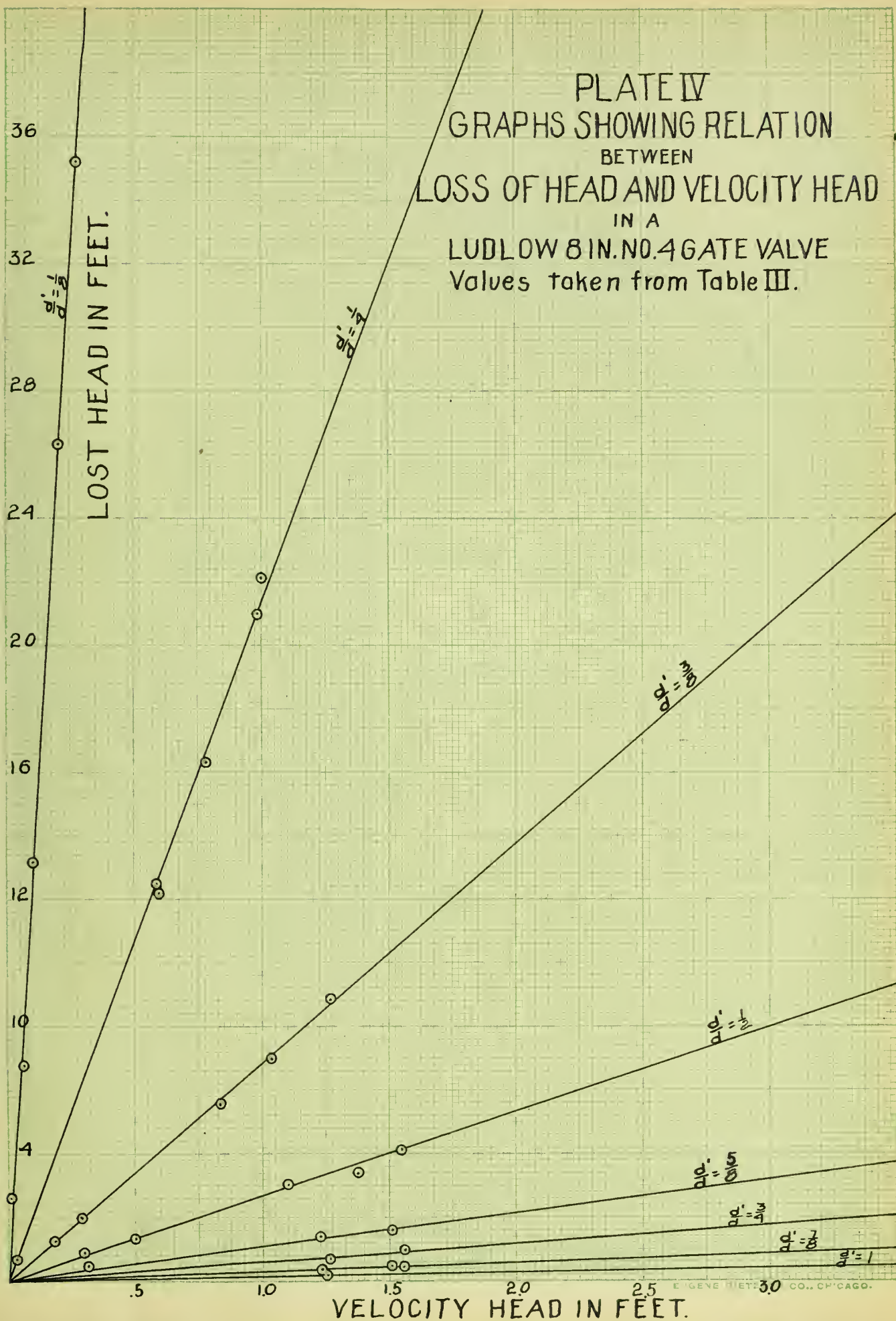


PLATE V
GRAPHS SHOWING RELATION
BETWEEN
PROPORTIONAL HEIGHT OF OPENING OF VALVE
AND
VALVE COEFFICIENT

- WEISBACH'S VALUES WITH 2 IN. VALVE.
- KUICHLING'S VALUES WITH 24 IN. VALVE.
- VALUES FROM TABLE II WITH 6 IN. VALVE.
- VALUES FROM TABLE IV WITH 8 IN. VALVE.

VALVE COEFFICIENT m

120
100
80
60
40
20

PROPORTIONAL HEIGHT OF OPENING OF VALVE.

$\frac{1}{2}$ $\frac{2}{3}$ $\frac{3}{4}$ $\frac{4}{5}$ $\frac{5}{6}$ $\frac{6}{7}$ $\frac{7}{8}$ $\frac{8}{9}$ $\frac{9}{10}$





UNIVERSITY OF ILLINOIS-URBANA



3 0112 082196681